



The 27th INTERNATIONAL  
ELECTRIC VEHICLE  
SYMPOSIUM & EXHIBITION  
BARCELONA  
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# Towards advanced BMS algorithms development for (P)HEV and EV by use of a physics-based model of Li-ion battery systems

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IFPEN, Lyon

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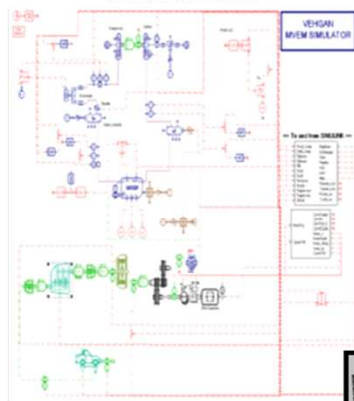


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**A complete approach is developed**

Vehicle and  
powertrain  
simulation

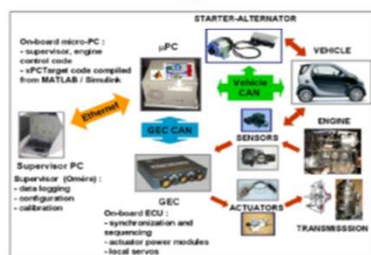
LMS AMESim



Real time  
simulation



Integrated  
powertrain  
control



Component  
testing and  
optimization

Energy storage  
system  
test bench

BMS



Engine test benches



Vehicle  
testing



Prototypes  
design,  
realization  
and  
optimization



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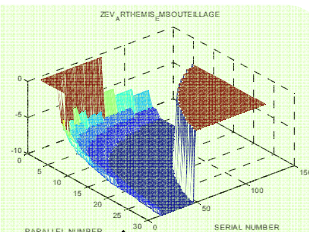
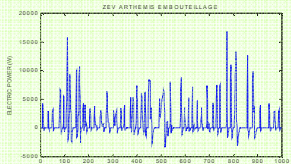
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## IFPEN R&D Electrochemical storage systems models

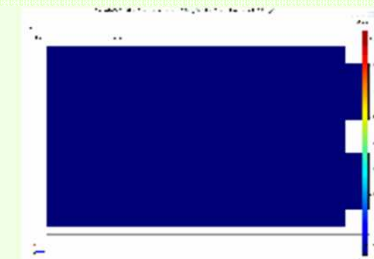
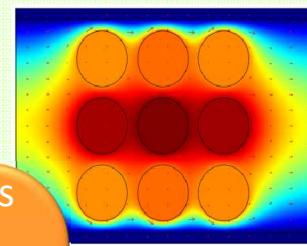
### Battery Pack Sizing



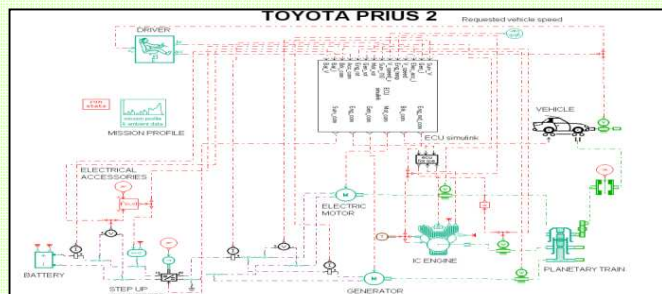
Power/Energy requirements  
or vehicle mission profiles  
Batch Simulations with  
cell constraints  
& vehicle constraints

Battery and supercapacitors  
characterization  
Multi-Physics & Multi-  
Dimensional Models  
Electrochemical models,  
Impedance-Based models  
Aging

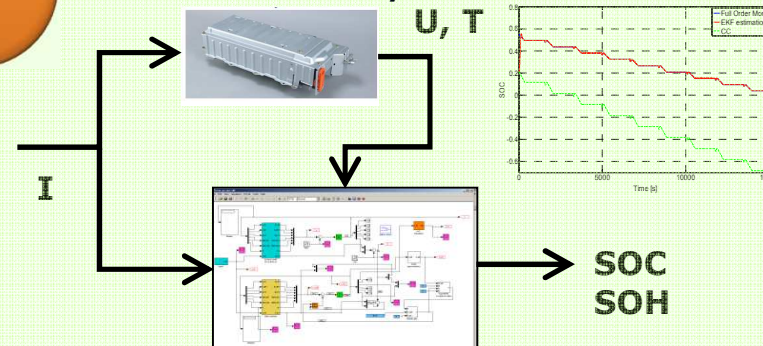
### Thermal Management laws



### HEV / PHEV / EV Simulators (Available LIBES software on AMESim)



### Model Based BMS estimators SOC / SOH U, T



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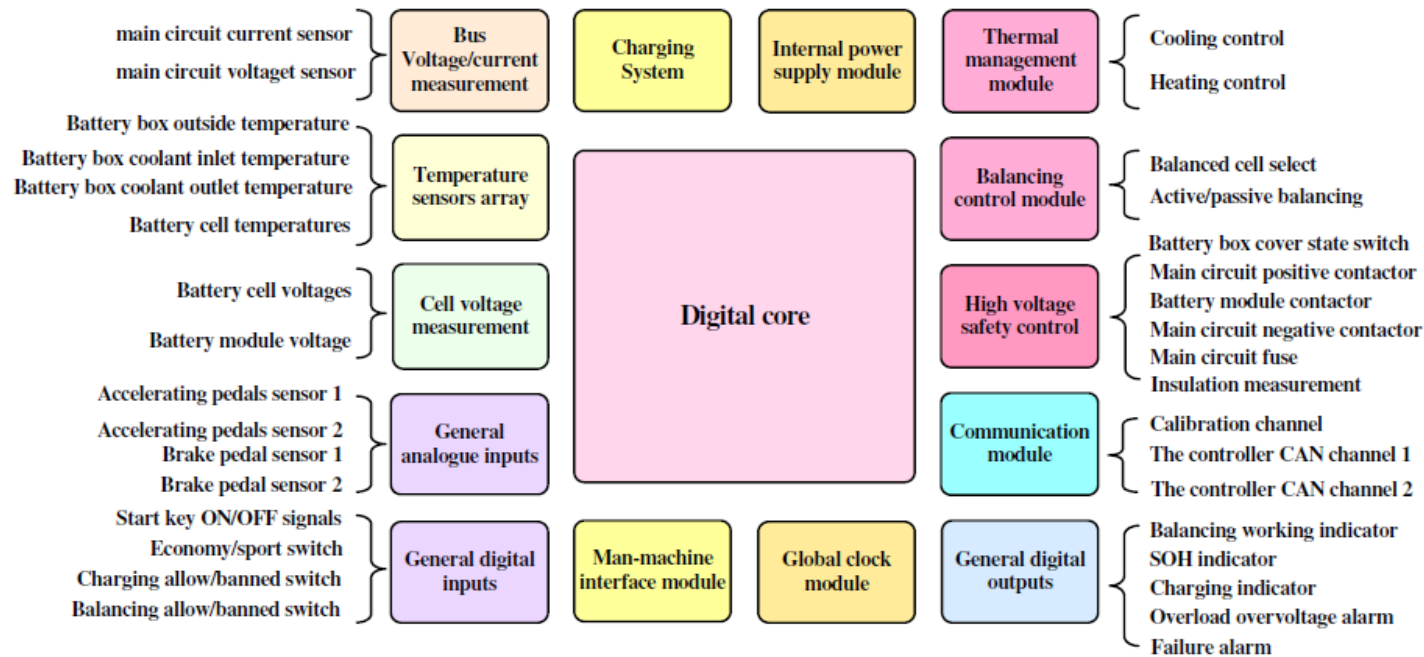


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- The battery management system (BMS) has to ensure reliable and safe use of stored electrical energy onboard (P)HEV and BEV
- Different functions to monitor the battery: SOC



➔ Herein, focus on a Battery Intensity Management Algorithm (BIMA) and the related methodology to design charge/discharge maximal intensity (CMI/DMI)

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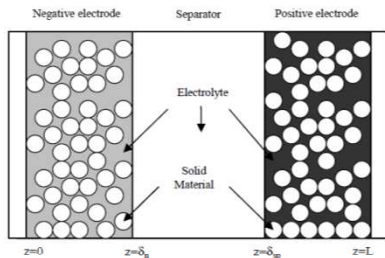


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# Modified SP Electro-thermal model Prada et al. JES 2013

## Hypotheses and modeling approach



The cell voltage ( $V$ ) is expressed:

1) as the sum of kinetics and mass transport overpotentials in the electrodes and electrolyte

2) as a function of the design parameters (Porosity, Electrodes thicknesses...) and physical properties of electrodes and electrolyte (Diffusion coefficients, Electrochemical kinetics...)

\*Hypotheses and Set of Equations can be found in Prada et al. JES 159 (9) A1508-A1519 (2012), "A Simplified Electrochemical and thermal model of LiFePO<sub>4</sub>-graphite Li-ion batteries for Fast Charge Applications"

## Thermal sub-model

$$\frac{dT_{skin}}{dt} = \frac{1}{mC_p} (Q_{irrev} + Q_{rev} - q_n) \quad \text{Energy Balance}$$

$$Q_{irrev} = -(V - (U_p - U_n))I \quad \text{Irreversible Thermal power (W)}$$

$$Q_{rev} = -T_{skin} \frac{d(U_p - U_n)}{dT} I \quad \text{Reversible Thermal power (W)}$$

$$q_n = h_{conv} S_{cell} (T_{skin} - T_{cooling}) \quad \text{Exchange Thermal power (W)}$$

$$T_{centre} = T_{skin} \left( 1 + \frac{h_{conv} S_{cell}}{\lambda_{cell} r_{cell}} \right) - T_{cooling} \frac{h_{conv} S_{cell}}{\lambda_{cell} r_{cell}} \quad \text{Internal temperature (K)}$$

## Electrochemical sub-model

### Cell Voltage ( $V$ )

$$V(t) = U_p \left( \frac{c_{s,p}^x}{c_{s,p,max}} \right) - U_n \left( \frac{c_{s,n}^x}{c_{s,n,max}} \right)$$

### State of Charge of the (+) and (-) electrodes (%)

$$\theta_p^x = \frac{c_{s,p}^x}{c_{s,p,max}} \quad \theta_n^x = \frac{c_{s,n}^x}{c_{s,n,max}}$$

$$+ \frac{RT}{\alpha F} \ln \left( \frac{-R_{s,p}}{6\varepsilon_{s,p} j_{0,p} A \delta_p} I + \sqrt{\left( \frac{R_{s,p}}{6\varepsilon_{s,p} j_{0,p} A \delta_p} I \right)^2 + 1} \right)$$

### State of Charge of the battery (%)

$$+ (1-t) \frac{2RT}{F} \ln \frac{c_a(L)}{c_a(0)} - \frac{I}{2A} \left( \frac{\delta_n}{\kappa_n^{\text{eff}}} + 2 \frac{\delta_{sep}}{\kappa_{sep}^{\text{eff}}} + \frac{\delta_p}{\kappa_p^{\text{eff}}} \right) - IR_{SEI}$$

$$SOC_{bat} = 100 \times \left( \frac{\theta_n^b - \theta_{n,0\%}^b}{\theta_{n,100\%}^b - \theta_{n,0\%}^b} \right)$$

## Modified SP Electro-Thermal model OUTPUT

Cell Voltage (V)

SOC<sub>bat</sub> (%)

T<sub>skin</sub> (K)

T<sub>centre</sub> (K)

A123  
Systems Cell,  
2,3 Ah



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- The Li-ion battery cell is a NCA/C
- The nominal capacity is 41Ah
- The cell is a mixed-typology for PHEV-EV
- Most of electrochemical and thermal model parameters are taken from literature data. Mass transport parameters are adjusted based on experimental tests
- Simulation results between experimental and model prediction at different continuous discharge rates (From manufacturer datasheet)



	Voltage (V)	Temperature (°C)
Maximum	4.1	60
Minimum	2.7	-25

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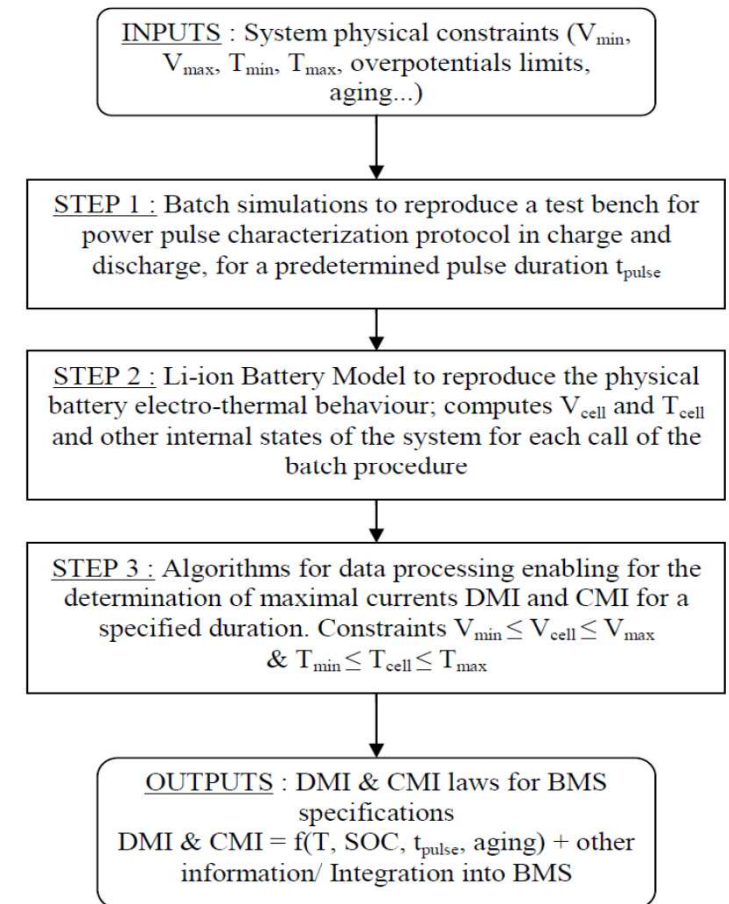
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## Model-based methodology (1/2)

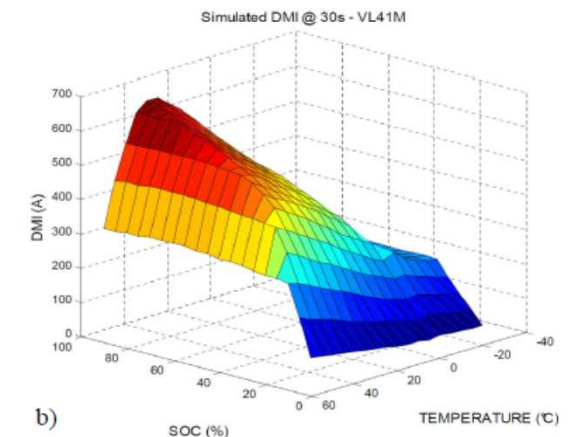
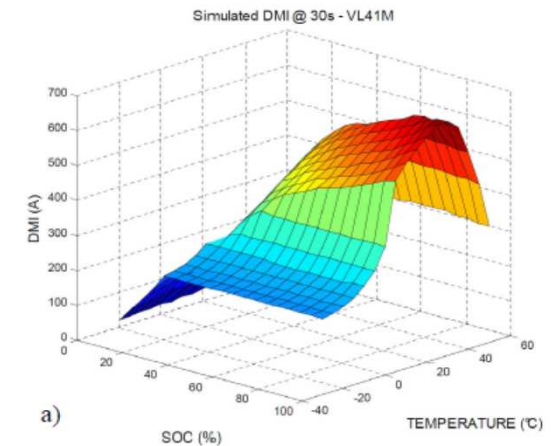
- Model-based methodology to design the allowable maximal charge and discharge current intensities (CMI & DMI)
- The battery electrochemical and thermal model is used as a virtual system to streamline experimental tests.
- The inputs are the cell voltage  $V_{cell}$  and temperature  $T_{cell}$  constraints (from manufacturer datasheet)

- Simulation & CMI) for a specified pulse duration

	Voltage (V)	Temperature (°C)
Maximum	4.1	60
Minimum	2.7	-25

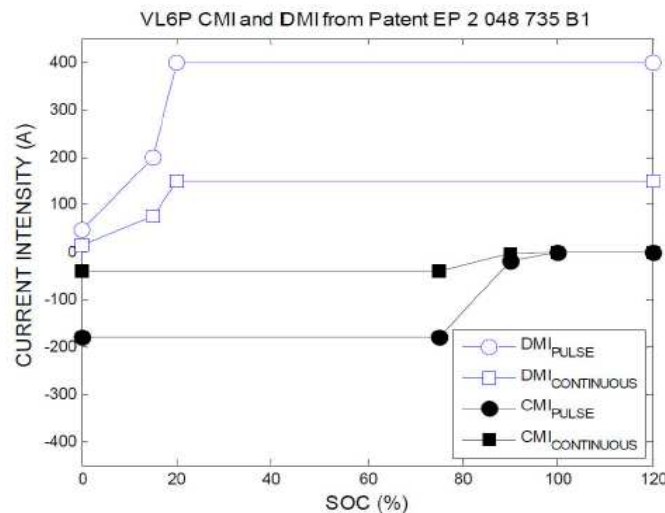


- Results of the Model-based methodology to design the allowable maximal charge and discharge current intensities
- For a given pulse duration, the output is a map representing maximal intensity as a function of SOC and T.
- The map shows different zones:
  - Voltage-induced limitation between 5° C and 35° C due to solid-state diffusion mechanism
  - Intensity-induced limitation above 35° C due to thermal constraints
  - Intensity-induced limitation below 5° C due to electrolytic-phase diffusion mechanism

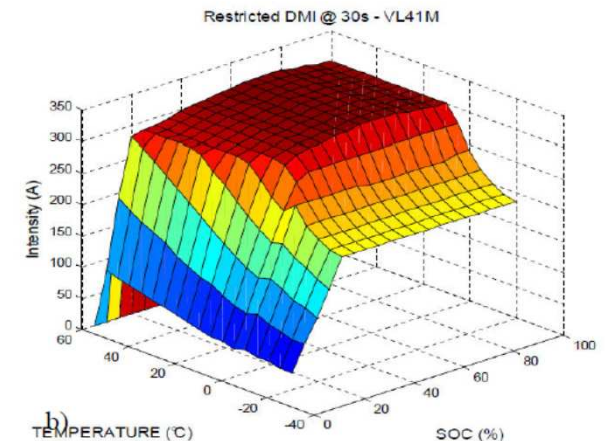
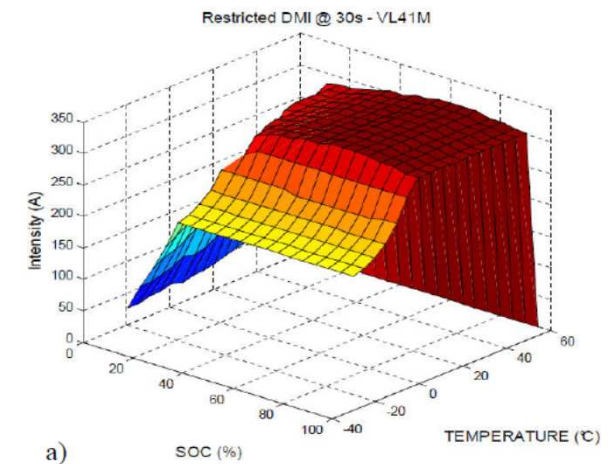


# Comparison with the manufacturer specifications

- For (P)HEV & BEV BMS, the simulations results are compared with the manufacturer specifications (for another Li-ion cell)



- Presence of current plateaus as well
- By restricting the map at 55° C values, one can observed similar trends as a function of SOC
- Conservative option of the manufacturer?



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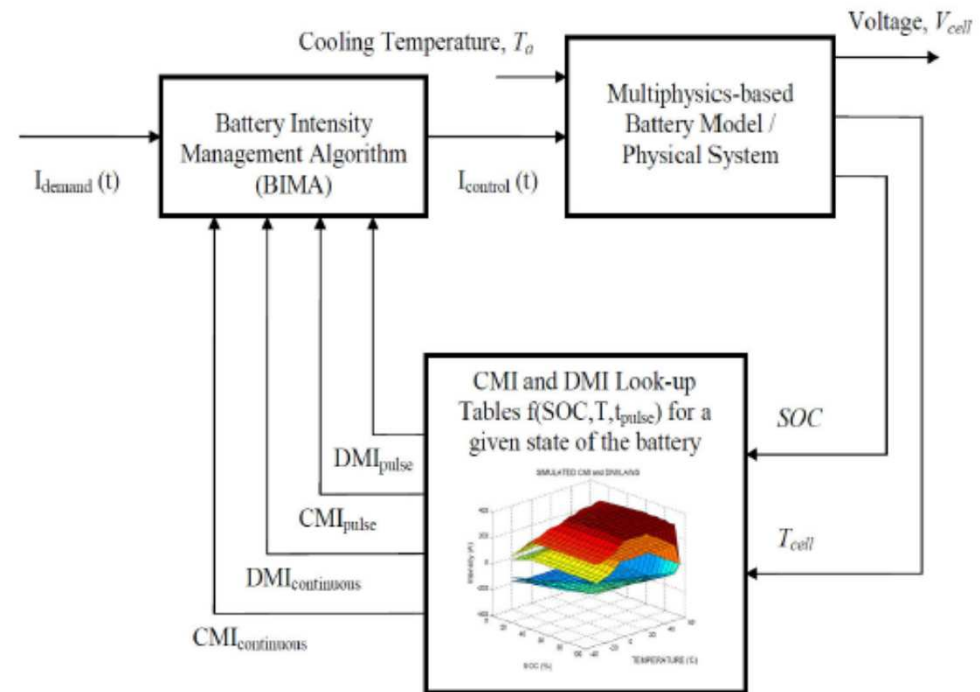
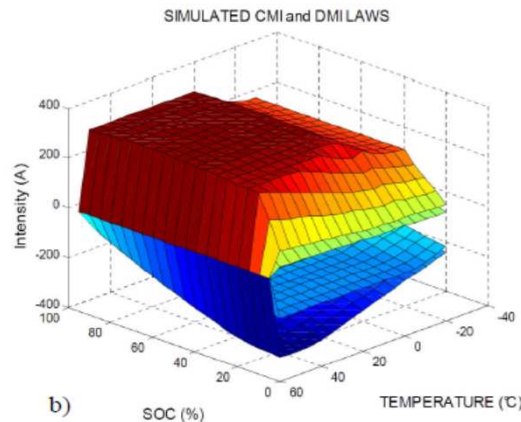
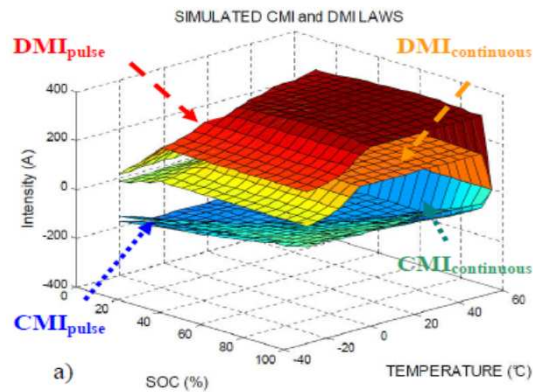


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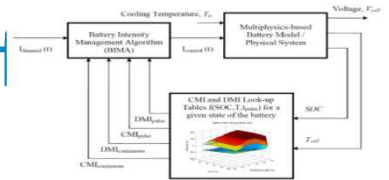
## Application of the methodology for (P)HEV & EV

- Design of restricted DMI and CMI laws for pulse and continuous operations



- Design of a BIMA controller fed by the DMI and CMI maps

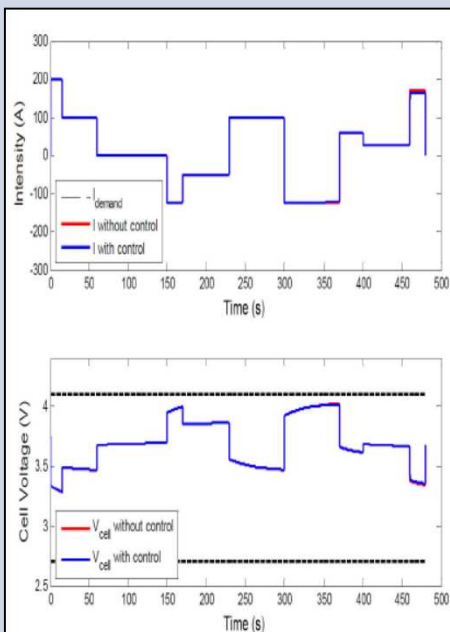
# Numerical validation of the BIMA



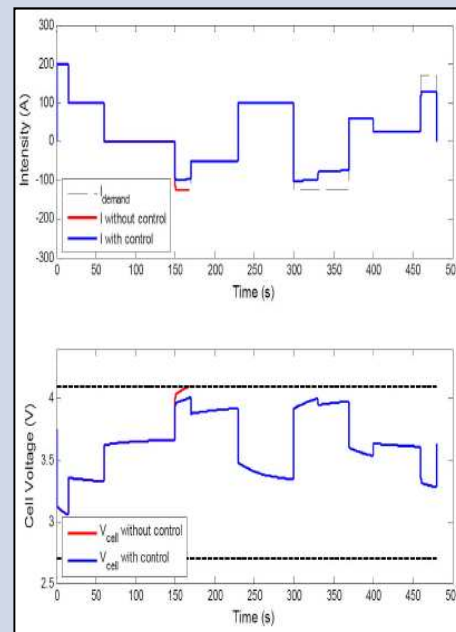
- Four cases are proposed to simulate different battery operations and to test the BIMA
- The demanded intensity is represented in dashed line, the intensity without control is in red line and the controlled intensity is in blue line.

Simulation Case	Initial SOC (%)	Initial Temperature (°C)
N°1	70	+ 35
N°2	70	- 5
N°3	10	+ 35
N°4	100	+ 35

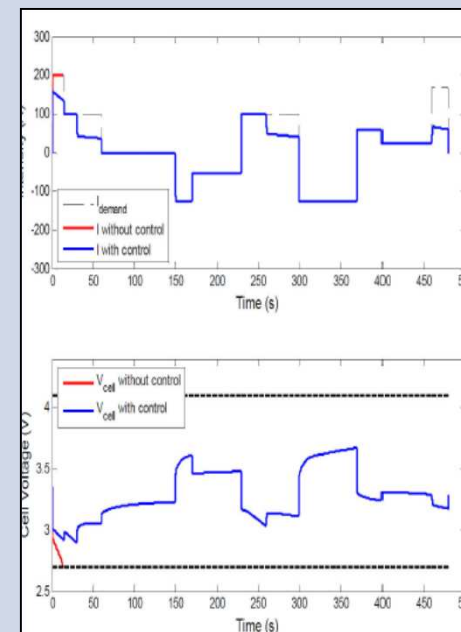
Nominal case



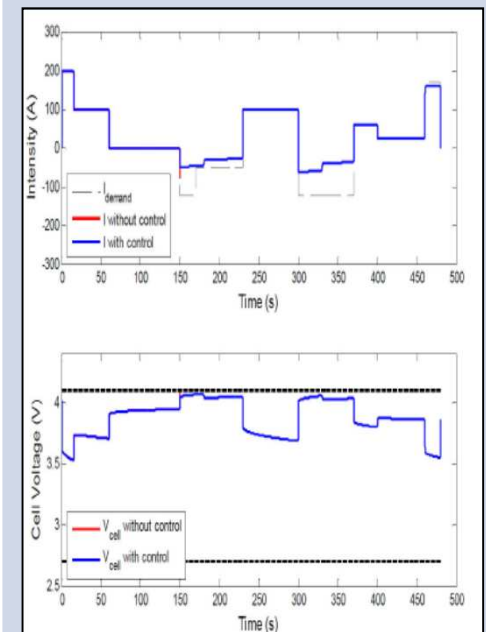
Cold Battery



Depleted Battery



Fully charged Battery



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- A model-based methodology to design the maps of allowable charge and discharge currents (CMI/DMI) for Li-ion batteries is presented and used for (P)HEV and BEV
- The methodology allows for a rapid prototyping of CMI and DMI laws based on a simplified electrochemical and thermal model
- The CMI and DMI maps feed a Battery Intensity Management Algorithm that is numerically tested and validated for different case studies.
- Future work will deal with the integration of aging adaption within the preliminary BIMA presented herein

➔ **Need of a generic multi-physics (electrochemical, thermal, mechanical) and multi-chemistry aging model for Li-ion technologies to extend the methodology**

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Feel free to contact us for any questions and for the upcoming AGIL(ES)<sup>2</sup>  
Consortium\*!

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\* AGIL(ES)<sup>2</sup> : AGing modeling of Industrial Li-ion Electrochemical Energy Storage Systems

# Thank you for your attention

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